

Please replace the paragraph beginning at page 13, line 5, with the following rewritten

paragraph:

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The porous peripheral surface provided in the tubular barrel may be anything provided that the surface-treating material can be reached to a work piece accommodated in the tubular barrel, including a mesh-formed peripheral surface as a representative thereof. The mesh-formed peripheral surface includes, for example, those made using a stainless-steel mesh net. The stainless-steel mesh net may be, for example, formed by a net-formed plate obtained by punching or etching a stainless steel plate, or formed by knitting stainless-steel linear members. Meanwhile, the porous peripheral surface may be a slit-formed peripheral surface. The slit-formed peripheral surface, for example, includes those made by arranging stainless-steel linear members in a stripe form with a gap. Furthermore, the porous peripheral surface may be a grating-formed peripheral surface. The opening ratio of the porous peripheral surface (ratio in area of the opening to the entire peripheral surface), although depending on the form and size of a work piece, is desirably 50% to 95%, and more desirably 60% to 85%. If the opening ratio is smaller than 50%, the peripheral surface acts as a barrier between the surface-treating material supply section and the work piece resulting in a fear of lowering the treatment efficiency. If the opening ratio is greater than 95%, there is a fear that the peripheral surface be deformed or damaged upon treating or handling thereof. In addition, the thickness of the peripheral surface is selected with considerations to the opening ratio or strength thereof, and desirably 0.1 mm to 10 mm. Further, more desirably 0.3 mm to 5 mm in consideration to easy handling.

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**Please replace the paragraph beginning at page 16, line 7, with the following rewritten paragraph:**

A3 The vertical section of the tubular barrel with respect to the rotational axis, preferably, is polygonal having at least three corners with an internal angle of  $30^{\circ}$  to  $100^{\circ}$ . More preferably, the form is polygonal having at least three corners with an internal angle of  $55^{\circ}$  to  $95^{\circ}$ . Particularly, the barrel having a triangular or rectangular section is well suited in respect of easy manufacture of the barrel. Furthermore, the barrel equal in angle at all the corners, e.g. the barrel having a section of a regular triangle or square, is particularly preferred because of capability of evenly, stably stopping the slide of the work piece at the corner and inverting the surfaces thereof at that point as a fulcrum. In the case that the length of the work piece is in relationship of equal to or greater than one-third of the one-side length of the polygon forming the section, the work piece can be efficiently inverted of surfaces at the corner, as a fulcrum, having an internal angle of  $30^{\circ}$  to  $100^{\circ}$ .

**Please replace the paragraph beginning at page 25, line 10, with the following rewritten paragraph:**

A4 The deposition apparatus shown in Fig. 4A exhibits the above effects and is convenient in respect of providing the below advantage.

**Please replace the paragraph beginning at page 26, line 18, with the following rewritten paragraph:**

A5 In addition, there is shown in the deposition apparatus of Fig. 4A a structure that the support members 57 supporting the tubular barrels 55 are disposed in the upper region of the vacuum-treating chamber 51 while the boat 52 as an evaporating section is in the lower region of the chamber, i.e. a structure for

deposition in one way toward the work pieces. However, the relationship between the support member and the evaporating section is not limited to this structure. It is preferred to properly determine the positional relationship or the number depending upon a work-piece treating amount and film forming condition.

**Please replace the paragraph beginning at page 27, line 4, with the following rewritten paragraph:**

Although the deposition apparatus shown in Fig. 4A has six tubular barrels 55 supported in one support member 57, the number of tubular barrels supported in the support member is not limited to that, i.e. one in the number is satisfactory. Furthermore, as shown in Figs. 4B and 4C, the shape of the tubular barrel can be a square or a rhombus, respectively.

**Please replace the paragraph beginning at page 27, line 13, with the following rewritten paragraph:**

The deposition apparatus shown in Fig. 5 is an apparatus with another structure. Fig. 5 is a diagrammatic front view (a partially perspective view) of an inside of a vacuum-treating chamber 101 of the same. This apparatus has two support members 107 juxtaposed, for rotation about a horizontal rotational axis 106 in an upper region of the vacuum-treating chamber 101 connected to an evacuating system, not shown. In the circumferential outward of the rotational axis of the support member, six tubular barrels 105 formed by mesh net of stainless steel having a rhombic vertical section with respect to the rotational axis are detachably attached in view of well handling thereof. The rhombic tubular barrel 105 has an interior divided symmetrically left and right into two by a partition formed by stainless-steel mesh net, to form partitioned chambers regular-triangular in vertical section with respect to the rotational axis. In order to provide even deposition treatment to the magnets 140 accommodated in the left and right

A7  
partitioned chambers, the left and right partitioned chambers are partitioned by a partition in a positional relationship having a rotational axis 106 on an extension between them (see the one-dot chain line in Fig. 5). In addition, the structure in the lower region of the chamber interior is similar to that of the deposition apparatus shown in Fig. 4A. By rotating the support member 107 about the rotational axis 106 (see the arrow in Fig. 5) it is possible to obtain an effect similar to that of the deposition apparatus shown in Fig. 4A.

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Please replace the paragraph beginning at page 29, line 1, with the following rewritten

paragraph:

A8  
Fig. 7 is a diagrammatic perspective view of the tubular barrel 125 having a vertical section of a convex lens with respect to the rotational axis to be used in the form shown in Fig. 6. The tubular barrel 125, to be opened and closed along a lengthwise direction, is made up by a lid 125a and a cage 125b structured for open and close through hinges, not shown, to have a support shaft 128 for supporting the barrel in the support member 127. Because the use of such a tubular barrel 125 facilitates the insertion and removal of work pieces, it is possible to suppress the work pieces from breakage or cracks upon insertion and removal thereof. In addition, where such a tubular barrel 125 is continuously used, there is a fear that a gap occurs between the lid 125a and the cage 125b due to deformation of the mesh net forming the barrel by the affection of thermal hysteresis in the deposition treatment thus resulting in falling off of the work pieces through the gap. It is accordingly preferred to attach a work-piece-fall preventing plate 129 to the cage 125b in a lengthwise direction of an opening thereof (the work-piece-fall

preventing plate 129 may be attached to the lid 125a in a lengthwise direction of the opening thereof).

During deposition treatment, the lid 125a and the cage 125b are fastened and used with a clip not shown.

A8  
The interior of the tubular barrel 125 is divided symmetrically left and right into two to form partitioned chambers. The partition 130 between the partitioned chambers is formed by stainless-steel mesh net. The partitioned chamber is divided into two by a spiral partitioning member 131 provided vertical to the rotational axis and formed by a stainless-steel linear member to have a gap therein. If work pieces are accommodated in the formed partitioned accommodation sections on a one-to-one basis to carry out deposition treatment to the work pieces in a spaced state, the work pieces can be smoothly inverted of surfaces at the slide stops as fulcrums without causing dispersion in deposition due to overlap between the work pieces or breakage or cracks due to collision between them. In addition, the lid 125a and the cage 125b may be structured completely separated without connection to be used by clip fastening when necessary instead of connection through the hinges, from the viewpoint of securing easy insertion and removal of work pieces and easy attachment and detachment of the partition 130 or spiral partitioning member 131.

IN THE CLAIMS:

Please amend claims 2-8, 10-20 and 23-26 as follows:

2. (Amended) An apparatus according to claim 1, wherein said tubular barrel has a sectional shape with respect to the rotational axis having at least one corner at an internal angle of 30° to 100°, said corner being provided as said slide stop.